



“Memoire sur les lois du mouvement des fluides”

Claude-Louis Navier

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Claude Navier - Biography

- ☀ Born: 10 Feb 1785 in Dijon, France----- Died: 21 Aug 1836 in Paris.**
- ☀ Education: Ecole Polytechnique in 1802 and Ecole des Ponts et Chaussées (1804)**
- ☀ Professor at Ecole des Ponts et Chaussées (1819) – applied mechanics**
- ☀ Elected to the Académie des Sciences in Paris in 1824**

“Navier believed in an industrialized world in which science and technology would solve most of the problems. “

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Professional profile

- ✿ Civil engineering (Emiland Gauthey)**
- ✿ Bridge construction**
- ✿ Survey and analysis of river flow**
- ✿ Engineering, elasticity and fluid mechanics**
- ✿ Contributions to Fourier series and their application to physical problems.**
- Work on modifying Euler's equations to take into account forces between the molecules in the fluid.**

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A short history of fluid dynamics

- 3rd B.C. , Archimedes, "On Floating Bodies"
- 15th Century, L. de Vinci, observations
- 1687, Newton in " Principia", viscosity force $\propto$ velocity variation
- 1738, D. Bernoulli, "Hydrodynamics"
- 1755, L. Euler, perfect flow, equations of continuity and momentum for frictionless fluids which are compressible or incompressible

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A short history of fluid dynamics

- 1821, C. Navier : derived Navier-Stokes equations, stress tensor
- 1829, S. Poisson, for viscous fluids
- 1845, G. Stokes, rederived Navier's results, formulated the non-slip boundary condition (considering friction but non-solvable mathematically)
- 1851, G. Stokes solved " a spherical particle moving through viscous liquids neglecting inertial forces"

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Context

From Euler (perfect flow)

$$\rho \frac{D\mathbf{u}}{Dt} = \rho \left(\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} \right) = -\nabla P,$$



To Navier (Viscous and incompressible flow)

$$\rho \left(\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} \right) = -\frac{\partial P}{\partial x} + \eta \left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right) + F_x$$

$$\rho \left(\frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} \right) = -\frac{\partial P}{\partial y} + \eta \left(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} + \frac{\partial^2 v}{\partial z^2} \right) + F_y$$

$$\rho \left(\frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} \right) = -\frac{\partial P}{\partial z} + \eta \left(\frac{\partial^2 w}{\partial x^2} + \frac{\partial^2 w}{\partial y^2} + \frac{\partial^2 w}{\partial z^2} \right) + F_z.$$



Navier's slip condition and general formulation

No-slip boundary condition to fluid flow over a solid surface



Validated by number of macroscopic flows but it remains an assumption based on physical principles.



Navier's proposed boundary condition assumes that the velocity, u_z , at a solid surface is proportional to the shear rate at the surface

shear rate at the
surface

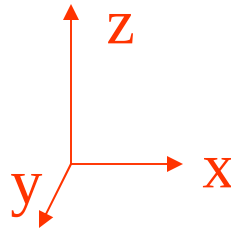
$$\eta \frac{\partial u_z}{\partial z} = \beta u_z$$

tangent component of
fluid velocity

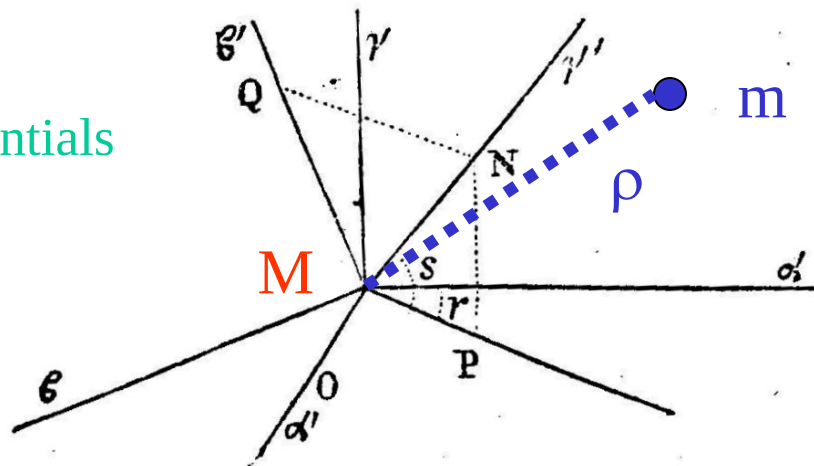


Calculation of the molecular forces developed by the fluid motion

- M is at the interface between wall and fluid (x,y,z)
- M velocity (u,v,w)



Referentials



- m is in the fluid:

$$\begin{cases} x + \alpha \\ y + C \\ z + \gamma \end{cases}$$

- m velocity:

$$\begin{cases} u + \frac{du}{dx}\alpha + \frac{du}{dy}\epsilon + \frac{du}{dz}\gamma, \\ v + \frac{dv}{dx}\alpha + \frac{dv}{dy}\epsilon + \frac{dv}{dz}\gamma, \\ w + \frac{dw}{dx}\alpha + \frac{dw}{dy}\epsilon + \frac{dw}{dz}\gamma, \end{cases}$$

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Calculation of the molecular forces developed by the fluid motion

Velocity of **m** moving away from **M** $\Rightarrow \frac{1}{\rho} (\alpha u + \beta v + \gamma w)$

If impulsion to **m**: Velocity of **m** $\Rightarrow \frac{1}{\rho} (\alpha \delta u + \beta \delta v + \gamma \delta w)$

Σ moment of action between molecule **m** and **M**, in Mm direction :

$$\frac{F(\rho)}{\rho^2} (\alpha u + \beta v + \gamma w) \cdot (\alpha \delta u + \beta \delta v + \gamma \delta w)$$

Action of the molecule **m** on **M**



Calculation of the molecular forces developed by the fluid motion

1. Integration on the half sphere
2. Referential change
3. Multiply by volume unit

4. Let's introduce:

$$\frac{4 \cdot \pi}{6} \int_0^\infty d\rho \cdot \rho^3 F(\rho) = E$$

Where E is a constant given by experiment and depending on the wall and fluid nature.

“E can be expressed as the reciprocal action wall/fluid” translated from Navier.

→ Σ moments generated by actions of all molecules **m**-like to **M**:

$$E(u \delta u + v \delta v + w \delta w)$$

5. $\int x \, ds^2$

6. Integration on the surface of the fluid



Calculation of the molecular forces developed by the fluid motion

6. General eq : Σ moments applied to incompressible fluid molecules = 0

density

acceleration force

now-called viscosity

$$0 = \iiint dx dy dz \left\{ \begin{aligned} &\left[P - \frac{dp}{dx} - \rho \left(\frac{du}{dt} + u \frac{du}{dx} + v \frac{du}{dy} + w \frac{du}{dz} \right) \right] \delta u \\ &\left[Q - \frac{dp}{dy} - \rho \left(\frac{dv}{dt} + u \frac{dv}{dx} + v \frac{dv}{dy} + w \frac{dv}{dz} \right) \right] \delta v \\ &\left[R - \frac{dp}{dz} - \rho \left(\frac{dw}{dt} + u \frac{dw}{dx} + v \frac{dw}{dy} + w \frac{dw}{dz} \right) \right] \delta w \end{aligned} \right\}$$

(Eq. 1)

$$- \epsilon \iiint dx dy dz \left\{ \begin{aligned} &3 \frac{du}{dx} \frac{\delta du}{dx} + \frac{du}{dy} \frac{\delta du}{dy} + \frac{du}{dz} \frac{\delta du}{dz} + \frac{dv}{dy} \frac{\delta du}{dx} + \frac{dv}{dx} \frac{\delta du}{dy} + \frac{dw}{dz} \frac{\delta du}{dx} + \frac{dw}{dx} \frac{\delta du}{dz} \\ &\frac{du}{dx} \frac{\delta dv}{dy} + \frac{du}{dy} \frac{\delta dv}{dx} + \frac{dv}{dx} \frac{\delta dv}{dx} + 3 \frac{dv}{dy} \frac{\delta dv}{dy} + \frac{dv}{dz} \frac{\delta dv}{dz} + \frac{dw}{dy} \frac{\delta dv}{dz} + \frac{dw}{dz} \frac{\delta dv}{dy} \\ &\frac{du}{dx} \frac{\delta dw}{dz} + \frac{du}{dz} \frac{\delta dw}{dx} + \frac{dv}{dy} \frac{\delta dw}{dz} + \frac{dv}{dz} \frac{\delta dw}{dy} + \frac{dw}{dx} \frac{\delta dw}{dx} + \frac{dw}{dy} \frac{\delta dw}{dy} + 3 \frac{dw}{dz} \frac{\delta dw}{dz} \end{aligned} \right\}$$

+ $S ds^2 \cdot E(u \delta u + v \delta v + w \delta w).$



From Eq. 1 => Navier's motion equation

1. Partial integration of eq. 1
2. Continuity equation

$$0 = \frac{du}{dx} + \frac{dv}{dy} + \frac{dw}{dz}$$



“Indefinite equations of motion”:

$$P - \frac{dp}{dx} = \rho \left(\frac{du}{dt} + u \frac{du}{dx} + v \frac{du}{dy} + w \frac{du}{dz} \right) - \epsilon \left(\frac{d^2 u}{dx^2} + \frac{d^2 u}{dy^2} + \frac{d^2 u}{dz^2} \right)$$

$$Q - \frac{dp}{dy} = \rho \left(\frac{dv}{dt} + u \frac{dv}{dx} + v \frac{dv}{dy} + w \frac{dv}{dz} \right) - \epsilon \left(\frac{d^2 v}{dx^2} + \frac{d^2 v}{dy^2} + \frac{d^2 v}{dz^2} \right)$$

$$R - \frac{dp}{dz} = \rho \left(\frac{dw}{dt} + u \frac{dw}{dx} + v \frac{dw}{dy} + w \frac{dw}{dz} \right) - \epsilon \left(\frac{d^2 w}{dx^2} + \frac{d^2 w}{dy^2} + \frac{d^2 w}{dz^2} \right)$$



From Eq. 1 => Navier's Slip condition

1. Referential change (l,m,n) angle with plan yz, xz and xy
2. Conditions to get $\delta u, \delta v, \delta w = 0$

$$Eu + \varepsilon \left[\cos.l \cdot 2 \frac{du}{dx} + \cos.m \left(\frac{du}{dy} + \frac{dv}{dx} \right) + \cos.n \left(\frac{du}{dz} + \frac{dw}{dx} \right) \right] = 0$$

$$Ev + \varepsilon \left[\cos.l \left(\frac{du}{dy} + \frac{dv}{dx} \right) + \cos.m \cdot 2 \frac{dv}{dy} + \cos.n \left(\frac{dv}{dz} + \frac{dw}{dy} \right) \right] = 0$$

$$Ew + \varepsilon \left[\cos.l \left(\frac{du}{dz} + \frac{dw}{dx} \right) + \cos.m \left(\frac{dv}{dz} + \frac{dw}{dy} \right) + \cos.n \cdot 2 \frac{dw}{dz} \right] = 0$$

3. No motion of the molecules perpendicular to the wall

$$0 = u \cdot \cos.l + v \cdot \cos.m + w \cdot \cos.n$$



From Eq. 1 $\Rightarrow$ Navier's Slip condition

$$Eu + \varepsilon \left(\cos.l. \frac{du}{dx} + \cos.m. \frac{du}{dy} + \cos.n. \frac{du}{dz} \right) = 0,$$

$$Ev + \varepsilon \left(\cos.l. \frac{dv}{dx} + \cos.m. \frac{dv}{dy} + \cos.n. \frac{dv}{dz} \right) = 0$$

$$Ew + \varepsilon \left(\cos.l. \frac{dw}{dx} + \cos.m. \frac{dw}{dy} + \cos.n. \frac{dw}{dz} \right) = 0$$

Example : If **M** is perpendicular to z axis



$$Eu + \varepsilon \frac{du}{dz} = 0, \quad Ev + \varepsilon \frac{dv}{dz} = 0$$

Similar to the common formulation



$$\eta \frac{\partial u_z}{\partial z} = \beta u_z$$



Extra slides for potential explanation

Referential

$$\alpha = \rho \cos. \psi \cos. \varphi$$

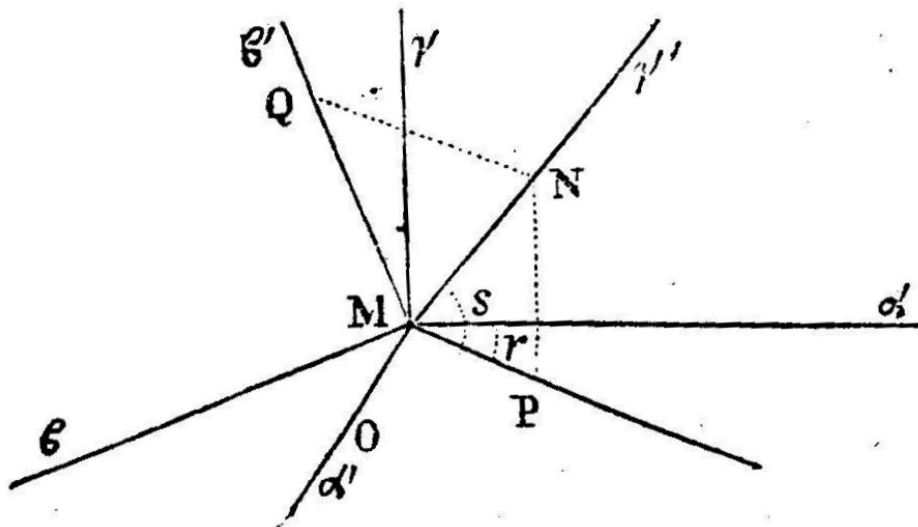
$$\epsilon = \rho \cos. \psi \sin. \varphi$$

$$\gamma = \rho \sin. \psi ;$$

$$\alpha' = \rho \cos. \psi \cos. \varphi$$

$$\epsilon' = \rho \cos. \psi \sin. \varphi$$

$$\gamma' = \rho \sin. \psi.$$



Point m definition:

$$u + \frac{du}{dx} \alpha + \frac{du}{dy} \epsilon + \frac{du}{dz} \gamma,$$

$$v + \frac{dv}{dx} \alpha + \frac{dv}{dy} \epsilon + \frac{dv}{dz} \gamma,$$

$$w + \frac{dw}{dx} \alpha + \frac{dw}{dy} \epsilon + \frac{dw}{dz} \gamma,$$



Extra slides for potential explanation

Velocity of m moving away from M $\Rightarrow \frac{I}{\rho} (\alpha u + \beta v + \gamma w)$

Impulsion to m $\Rightarrow \frac{I}{\rho} (\alpha \delta u + \beta \delta v + \gamma \delta w)$

Moments of reciprocal actions are:

$$\frac{I}{\rho^2} (\alpha u + \beta v + \gamma w) \cdot (\alpha \delta u + \beta \delta v + \gamma \delta w).$$

Sum of moments:

$$\frac{F(\rho)}{\rho^2} (\alpha u + \beta v + \gamma w) \cdot (\alpha \delta u + \beta \delta v + \gamma \delta w)$$



Extra slides for potential explanation

Integration to the half sphere:

$$\frac{4 \cdot F(\rho)}{\rho^2} \left\{ \begin{array}{l} \alpha'^2 \left\{ \begin{array}{l} (u \sin.^2 r - v \sin. r \cos. r) \delta u \\ (-u \sin. r \cos. r + v \cos.^2 r) \delta v \end{array} \right\} \\ \beta'^2 \left\{ \begin{array}{l} (u \cos.^2 r \sin.^2 s + v \sin. r \cos. r \sin.^2 s + w \cos. r \sin. s \cos. s) \delta u \\ (u \sin. r \cos. r \sin.^2 s + v \sin.^2 r \sin.^2 s + w \sin. r \sin. s \cos. s) \delta v \\ (u \cos. r \sin. s \cos. s + v \sin. r \sin. s \cos. s + w \cos.^2 s) \delta w \end{array} \right\} \\ \gamma'^2 \left\{ \begin{array}{l} (u \cos.^2 r \cos.^2 s + v \sin. r \cos. r \cos.^2 s - w \cos. r \sin. s \cos. s) \delta u \\ (u \sin. r \cos. r \cos.^2 s + v \sin.^2 r \cos.^2 s - w \sin. r \sin. s \cos. s) \delta v \\ (-u \cos. r \sin. s \cos. s - v \sin. r \sin. s \cos. s + w \sin.^2 s) \delta w \end{array} \right\} \end{array} \right\}$$

$$E(u \delta u + v \delta v + w \delta w)$$

$$\text{with } \frac{4 \cdot \pi}{6} \int_0^\infty d\rho \cdot \rho^2 F(\rho) = E$$